

# 椭圆锥稳燃器对煤粉火焰的稳燃作用

(华北电力大学)荆有印 王保生

**摘要:** 引入气固两相流的特性参数,从煤粉气流结构出发,分析了椭圆锥稳燃器对煤粉火焰的稳燃作用。

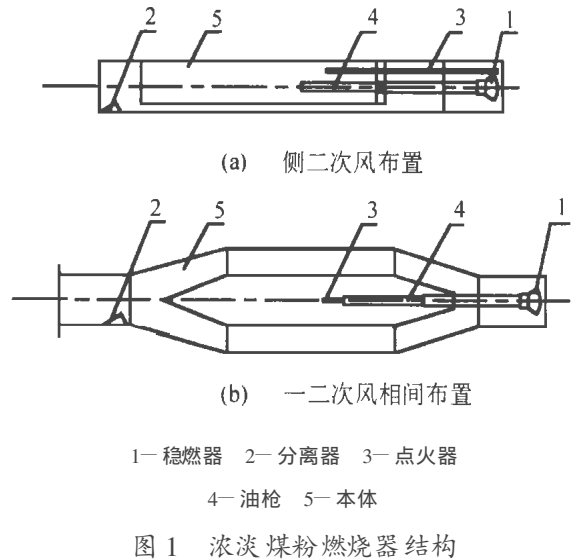
**关键词:** 椭圆锥稳燃器; 特性参数; 煤粉火焰; 着火和稳燃

中图分类号: TK223.23·0643.134

## 1 前言

根据燃烧理论,煤粉的着火和燃烧,实际上是挥发份和细煤粉颗粒在高温下的均相或非均相着火和稳燃问题。煤粉的着火和稳燃决定于在燃烧器喷口附近气固两相流的气流结构及煤粉的浓度和温度。温度越高,挥发份越易析出,煤粉浓度越高,挥发份析出越多,越易着火和稳燃。为了保证煤粉火焰的稳定燃烧,组织良好的炉内气流结构,使之形成煤粉着火的有利区,即所谓的“三高”稳燃区。浓淡煤粉椭圆锥燃烧器正是致力于此,集浓淡分离和钝体燃烧技术于一身,在一五〇电厂首次试验成功,并应用于呼市电厂和冀东水泥厂自备电厂。燃烧器结构如图1所示,在一次风管道出口处加装分离器,在一次风喷口内设置椭圆锥稳燃器,煤粉气流首先经分离器进行浓淡分离,使一次风喷口内向火侧煤粉气流增浓,流经稳燃器后收缩形成内外回流区,主射流形似拉法尔曲线。由于惯性力的作用,使煤粉在外回流区富集。煤粉在外回流区受上游高温烟气的加热,挥发分绝大部分已经析出,形成稳定的着火源,点燃煤粉,使火焰逐渐扩展到主射流区。高温促使挥发的析出和煤粉的着火,使煤粉火焰具有较强的

稳定性。试验表明:该燃烧器具有低负荷稳燃和少油点火功能,可在35%~50%额定负荷下脱油稳燃,冷态启动点火节油40%~50%,冀东水泥厂自备电厂飞灰含碳量由改造前的7%~9%降到3%左右。为了从理论上探讨椭圆锥稳燃器对煤粉火焰的稳燃作用,引入气固两相流特性参数。



## 2 煤粉气流特性参数

### 2.1 质量流量

煤粉空气混合物的质量流量  $G_h$  等于煤粉的质量流量  $G''$  和空气的质量流量  $G'$  之和:

$$G_h = G'' + G' \quad \text{kg/s} \quad (1)$$

煤粉空气混合物的容积流量  $V_h$  等于煤粉的容积流量  $V''$  和空气的容积流量  $V'$  之和:

$$V_h = V'' + V' \quad \text{m}^3/\text{s} \quad (2)$$

收稿日期: 1998-12-30; 修订日期: 1999-05-24

作者简介: 荆有印(1953-), 男, 山西朔州市人, 华北电力大学动力工程系高级工程师. 邮编 071003 河北保定

$$\text{或 } G_h/\rho_h = G''/\rho'' + G'/\rho' \quad (3)$$

式中:  $\rho_h, \rho'', \rho'$  —— 煤粉空气混合物、煤粉、空气的密度,  $\text{kg}/\text{m}^3$ 。

### 2.2 折算速度

假想煤粉空气混合物中的煤粉单独流过整个管道横截面时的速度称为煤粉的折算速度  $W_0''$ :

$$W_0'' = G''/\rho''f = V''/f \quad \text{m/s} \quad (4)$$

同理, 假想煤粉空气混合物中的空气单独流过整个管道横截面时的速度称为空气的折算速度  $W_0'$ :

$$W_0' = G'/\rho'f = V'/f \quad \text{m/s} \quad (5)$$

式中:  $f$  —— 管道横截面积,  $\text{m}^2$ 。

在煤粉管道中, 沿管长气固两相的质量流量不变, 即  $G'' = \text{const}$  和  $G' = \text{const}$ 。

### 2.3 质量流速

煤粉空气混合物的质量流速  $\rho_h W_h$  等于煤粉的质量流速  $\rho''W_0''$  和空气的质量流速  $\rho'W_0'$  之和:

$$\rho_h W_h = \rho''W_0'' + \rho'W_0' \quad \text{kg}/\text{m}^2\text{s} \quad (6)$$

### 2.4 容积含粉率和截面含粉率

在煤粉空气混合物中, 煤粉的容积流量与煤粉空气混合物的容积流量之比称为煤粉的容积含粉率  $\beta$ :

$$\beta = V''/V_h = W_0''/W_h \quad (7)$$

在某一管道截面上, 煤粉所占的截面积  $f''$  与整个管截面积  $f$  之比称为截面含粉率  $\varphi$ :

$$\varphi = f''/f \quad (8)$$

则空气所占的截面积比为:

$$f'/f = (f - f'') = 1 - \varphi \quad (9)$$

若以  $W''$  和  $W'$  代表煤粉和空气的真实速度, 则由  $f'' = V''/W''$ ,  $f' = V_h/W_h$ , 可得:

$$\varphi = f''/f = W_h V''/W'' V_h = C\beta \quad (10)$$

式中:  $C$  表示煤粉空气混合物的速度与煤粉的真实速度之比, 它反映了煤粉、空气之间由于存在相对速度而对截面含粉率的影响。在垂直上升管中, 由于重力的作用,  $W'' < W'$ ,  $\varphi > \beta$ ; 在垂直下降管中, 由于重力的作用,  $W'' > W'$ ,  $\varphi < \beta$ ; 当  $W'' = W'$  时,  $\varphi = \beta$ 。

### 2.5 煤粉浓度

在煤粉空气混合物中, 煤粉的质量流量与空气质量(或容积)流量之比称为煤粉的输送浓度  $\rho_m$ (或  $\rho_Q$ ):

$$\rho_m = G''/G' = \rho''W_0''/\rho'W_0' \quad \text{kg}/\text{kg} \quad (11)$$

$$\rho_Q = G''/V' = \rho''W_0''/W_0' \quad \text{kg}/\text{m}^3 \quad (12)$$

在煤粉空气混合物中, 煤粉的质量流量与空气混合物容积流量之比称为煤粉的空间浓度  $\rho_v$ :

$$\rho_v = G''/V_h = \rho''W_0''/W_h \quad \text{kg}/\text{m}^3 \quad (13)$$

煤粉的输送浓度与煤粉的空间浓度的关系:

$$\rho_v = \rho_Q/[W''\varphi/W'(1-\varphi)+1] = \rho_m\rho'/[W''\varphi/W'(1-\varphi)+1] \quad (14)$$

在燃烧系统中, 煤粉的输送浓度较低, 又由于煤粉很细, 输送力远大于重力的影响, 因此可认为  $\varphi \approx 1$ ,  $W'' \approx W'$ 。于是

$$\rho_v = \rho_Q = \rho_m\rho' \quad (15)$$

### 3 椭圆锥稳燃器对煤粉气流浓度的影响

如图 2 所示, 在燃烧器出口处, 由于椭圆锥稳燃器的作用, 使煤粉气流收缩, 形成内外回流区, 主射流形似拉法尔曲线。煤粉在惯性力的作用下, 富集于外回流区。在 2-2 截面处, 主射流区煤粉气流的速度增加, 两侧回流区煤粉气流的速度显著降低。由于煤粉质量守恒, 则燃烧器出口 1-1 截面处的煤粉气流与在 2-2 截面处的煤粉气流存在如下关系:

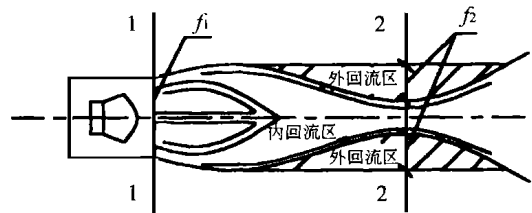


图 2 煤粉气流特性

$$\rho_{v1} W_1 f_1 = \rho_{v2} W_2 f_2 \quad \text{kg}/\text{s} \quad (16)$$

根据试验结果, 可近似的认为  $f_1 = f_2$ , 则

$$\rho_{v2} = \rho_{v1} W_1/W_2 \quad \text{kg}/\text{m}^3 \quad (17)$$

因为  $W_2 < W_1$ , 所以  $\rho_{v2} > \rho_{v1}$ , 试验结果表明

$$W_1/W_2 = 4 \sim 6$$

### 4 回流区煤粉浓度对火焰稳定性的影响

在内回流区, 烟气温度较低, 约  $100^{\circ}\text{C} \sim 300^{\circ}\text{C}$ ; 在外回流区, 煤粉富集, 由于相邻燃烧器喷射过来的高温烟气, 以及自身卷吸的高温烟气, 使该区的烟气温度约在  $900^{\circ}\text{C}$  以上, 在此形成所谓的“三高”稳燃区。在区域内煤粉浓度高, 着火热少, 挥发分绝大部分已析出, 为燃烧过程提供了良好的热力条件。可燃混合物在该区域内燃烧时放出热量, 同时也向周围介质吸热和散热, 吸热和散热在不同的条件下发生热平衡现象。下面以煤粉空气混合物在该区域内的热平衡情况来说明回流区煤粉浓度对火焰稳定性的影响。

挥发分燃烧反应放出的热量:

$$Q_1 = Q_{hf} V' V_h \rho_m \rho' \quad \text{kJ/s} \quad (18)$$

加热混合物本身消耗的热量:

$$Q_2 = V_h \rho_m \rho' C_p (T - T_0) \quad \text{kJ/s} \quad (19)$$

吸收上游高温烟气的热量:

$$Q_3 = S_1 \alpha_{d1} (T_1 - T_0) + \sigma S_1 \alpha_{f1} (T_1^4 - T_0^4) \quad \text{kJ/s} \quad (20)$$

传递给主射流的热量:

$$Q_4 = S_2 \alpha_{d2} (T - T_0) + \sigma S_2 \alpha_{f2} (T^4 - T_0^4) \quad \text{kJ/s} \quad (21)$$

热平衡式为:

$$Q_{hf} V' V_h \rho_m \rho' + S_1 \alpha_{d1} (T_1 - T_0) + \sigma S_1 \alpha_{f1} (T_1^4 - T_0^4) - V_h \rho_m \rho' C_p (T - T_0) - S_2 \alpha_{d2} (T - T_0) - \sigma S_2 \alpha_{f2} (T^4 - T_0^4) = 0 \quad (22)$$

整理后得:

$$\rho_m = \frac{S_1 \alpha_{d1} (T_1 - T_0) + \sigma S_1 \alpha_{f1} (T_1^4 - T_0^4) - S_2 \alpha_{d2} (T - T_0) - \sigma S_2 \alpha_{f2} (T^4 - T_0^4)}{V_h \rho' [C_p (T - T_0) - Q_{hf} V']} \quad (23)$$

由式(23)可绘出如图 3 所示的特性曲线  $\rho_m = f(V', T)$ 。

由图 3 可以看出: 当回流区烟气温度  $T$  增加时,

煤粉着火浓度  $\rho_m$  下降; 当挥发分  $V'$  下降时, 煤粉着火浓度  $\rho_m$  增加。也就是说, 当回流区煤粉浓度  $\rho_m$  增加时, 煤粉的着火温度下降; 当回流区煤粉浓度  $\rho_m$  或回流区烟气温度  $T$  增加时, 可燃用低挥发分煤粉。在椭圆锥稳燃器的作用下, 煤粉富集于外回流区, 使该区的煤粉增浓, 为迅速着火和稳定燃烧创造了良好的热力条件。

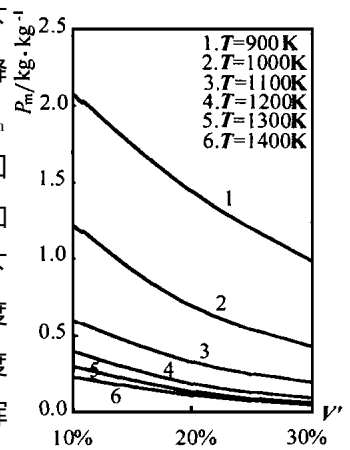


图 3  $\rho_m = f(V', T)$  特性曲线

### 5 结论

- (1) 椭圆锥稳燃器使煤粉气流收缩, 形成内外回流区。由于惯性力的作用, 使外回流区煤粉增浓, 对煤粉火焰具有较强的稳燃作用。
- (2) 浓淡煤粉椭圆锥燃烧器集浓淡分离和钝体燃烧于一身, 浓煤粉位于向火侧, 淡煤粉位于背火侧, 进一步强化了煤粉气流的加热、着火和燃烧过程。

### 参考文献

- [1] 徐旭常. 燃烧理论与燃烧设备. 北京: 机械工业出版社, 1990.
- [2] 何佩赵, 赵仲琥, 秦玉琨编. 煤粉燃烧器设计及运行. 北京: 机械工业出版社, 1987.
- [3] 胡荫平, 贾鸿祥编. 新型燃烧器. 西安: 西安交通大学出版社, 1993.
- [4] 李之光, 范柏樟主编. 工业锅炉手册. 天津: 天津科学技术出版社, 1988.
- [5] 徐秀清, 王云山等. 直流煤粉燃烧器出口“三高稳燃区”内煤粉的浓缩现象. 中国电力, 1997, (11).

(渠源 编辑)

ICR 进展及关键技术 = **New Developments in ICR Engines and Related Key Techniques** [刊, 中] / Liu Yongbao, Zhang Renxing (Naval Engineering Academy) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 415 ~ 418

In addition to a series of advantages specific to a simple cycle gas turbine ICR engines feature an excellent off-design performance with Model WR-21 engine being ranked as the most advanced. This paper gives a brief description of some new developments in WR-21 gas turbines. The key techniques relating to such major components as intercoolers, regenerators, engine enclosures and digital control systems are also analyzed. **Key words:** ICR gas turbine, intercooler, regenerator, enclosure, control system

气体燃料再燃对 NO<sub>x</sub> 还原的影响 = **Effects of Gaseous Fuel Reburning on NO<sub>x</sub> Reduction** [刊, 中] / Zhong Beijing, Fu Weibiao (Qinghua University) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 419 ~ 423

Gaseous fuel reburning pertains to one of the most effective methods being extensively studied for the reduction of NO<sub>x</sub> content in flue gases. With the gases in a typical primary combustion zone serving as simulation gases the authors have studied the influence of different gaseous fuels (CH<sub>4</sub>, C<sub>2</sub>H<sub>2</sub> and C<sub>2</sub>H<sub>4</sub>) and the reburning zone combustion conditions (excess air coefficient and reburning temperature) on NO<sub>x</sub> reburning process and its reduction. Through calculations it is found that different compositions of gaseous fuels, the excess air coefficient and firing temperature in the reburning zone exercise a significant influence on the NO<sub>x</sub> reburning process and NO<sub>x</sub> reduction rate. **Key words:** fuel reburning, gaseous fuel, NO<sub>x</sub> reduction

煤粉锅炉炉膛燃烧、传热一维数学模型的研究 = **A Study of the Combustion and Heat Transfer One-dimensional Mathematical Model for a Pulverized Coal-fired Boiler Furnace** [刊, 中] / Dong Peng, Hong Mei, Qin Yukun et al (Harbin Institute of Technology) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 424 ~ 427

A combustion and heat transfer one-dimensional mathematical model has been set up for the analytical computation of one-dimensional distribution magnitudes of such thermodynamic parameters as furnace gas temperatures, water wall absorption heat flux density, heat release rate, etc. under various operating conditions. The calculation and analysis of three different models of boilers and a comparison of the calculated results with original design data have validated the rationality of the adopted mathematical model. **Key words:** furnace internal process, in-furnace heat transfer, mathematical model, pulverized coal combustion

折焰角结构对上部炉膛流场影响的数值研究 = **Numerical Simulation of the Effect of Arch Nose Structure on Furnace Upper Section Flow Field** [刊, 中] / Li Yanpeng, Xu Jinyuan (Xi'an Jiaotong University) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 428 ~ 430

Based on a porosity conception conducted is a numerical simulation of the flow field in a boiler furnace under various arch nose structures. The effects of such structures on the residual swirl at the furnace outlet and the velocity distribution at the inlet of horizontal gas-pass were studied. The study results have been verified by way of a cold-state simulation test. They can serve as useful reference data during the design and retrofitting of utility boilers. **Key words:** arch nose, residual swirl, thermal excursion, numerical simulation

椭圆锥急燃器对煤粉火焰的稳燃作用 = **The Combustion Stabilizing Role Played by an Ellipsoidal Cone Combustion Stabilizer** [刊, 中] / Jing Youyin, Wang Baosheng (North China Electrical Power University) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 431 ~ 433

By introducing the characteristics parameters of a gas-solid two-phase flow and proceeding from the structure of a pulverized-coal flow an analysis is performed of the combustion stabilizing action of an ellipsoidal cone combustion stabilizer on a pulverized-coal flame. **Key words:** ellipsoidal cone combustion stabilizer, characteristics parameter, pulverized-coal flame, ignition and steady combustion

600MW 锅炉机组膜式水冷壁壁温的试验研究及理论分析 = **Experimental Investigation and Theoretical Analysis of Membrane Water Wall Temperature in a 600 MW Boiler Unit** [刊, 中] / Yu Yanzhi, Tang Biguang, Liu Yong, et al (Wuhan University of Water Resources and Electrical Power) // Journal of Engineering for Thermal Energy & Power. — 1999, 14(6). — 434 ~ 436