

# 两相流超音速流动、激波及其应用研究

赵良举, 曾丹苓

(重庆大学 动力工程学院, 重庆 400044)

**摘要:** 从两相流体的音速特点出发, 研究两相超音速流动, 分析超音速流动导致的激波状况, 并利用两相激波加速凝结和增压的特点, 设计了增压换热器。两相流的音速受其压缩性的影响而呈现出与单相流不同的特点, 其较小的音速值使得两相超音速流动更易实现。两相流激波与波前马赫数密切相关, 波后汽相凝结、压力升高, 利用该特点设计的汽水直接接触式换热器, 具有高效换热和增压的特点。

**关键词:** 汽液两相流; 超音速; 激波; 增压换热器

中图分类号: O359<sup>+1</sup> 文献标识码: A

## 1 引言

汽液两相流体的音速与可压缩性密切相关, 其可压缩性随空泡率的变化而发生显著的变化, 因而极大的影响了两相流体的音速。汽液两相流体中的音速远低于其中任何一种单相流体, 当空泡率在 50% 时, 其音速仅为几十米每秒。两相流体的低音速特点使两相流动显示出与单相流体不同的特性, 且两相间的换热情况对两相超音速流的流动参数有较大的影响。超音速流动可能导致激波, 两相流体的激波与单相理想气体有较大的差别。根据两相流体的以上特性, 可以设计一种增压型高效换热器, 在实现高效换热的同时实现增压的目的。

## 2 两相流音速

音速在可压缩流体流动过程的分析中至关重要, 为简化分析, 一般把声波传播视为一可逆绝热过程, 音速可用 Laplace 方程表示为  $a_s = \sqrt{(\partial p / \partial p)_s}$ 。对非定温有相变的气—液两相流体流动过程, 流体中不等温传热、粘性摩擦及非平衡相转变等不可逆因素的存在将对声波的传播带来不可忽略的影响。

文献[1]在充分考虑以上各种不可逆因素的情况下, 应用非平衡热力学理论导出实际音速的表达式, 并分别以空气及水及其蒸汽的混合物为例分析各不可逆因素对音速的影响。

研究发现, 对于单相理想气体, 在低频(包括可闻声)时, 导热、粘性对音速的影响很小, 可以不考虑, 而用 Laplace 公式计算音速。在高频( $> 1 \times 10^7$  Hz)时, 导热和粘性将使音速增加, 粘性影响更大, 同时考虑两者的影响音速值增加更多。对于两相流体(汽水混合物), 在低频(包括可闻声)时, 虽然导热、粘性对音速的影响很小, 但相变的影响较大, 可以不考虑导热和粘性的影响, 只考虑相变对音速的影响。在高频( $> 1 \times 10^7$  Hz)时, 随着频率的增加, 粘性和导热的影响增加。本文引入了相变弛豫系数  $\theta$  来度量相变对音速  $a$  的影响,

$$\begin{aligned} a^2 = & -v^2 [ (v'' - v') \theta (\frac{\partial x}{\partial p})_s + x \frac{dv''}{dp} + \\ & (1-x) \frac{dv'}{dp} ]^{-1} \end{aligned} \quad (1)$$

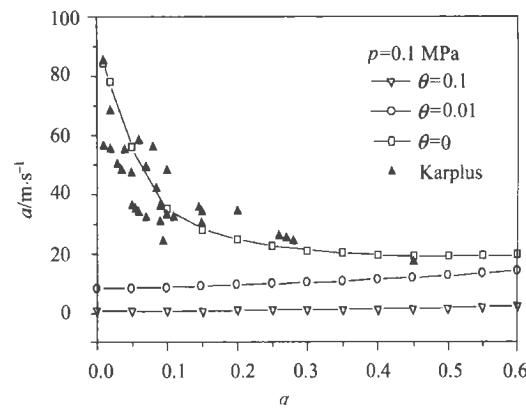


图 1 与 Karplus 实验值的比较

用式(1)计算的音速值与实验值的对比, 如图 1

和图2所示, 实验数据与  $\theta = 0$  的相冻结情况较为接近, 而与  $\theta = 1$  的充分相变(平衡相变)情况差别较大。这充分说明相变弛豫现象对音速的影响。

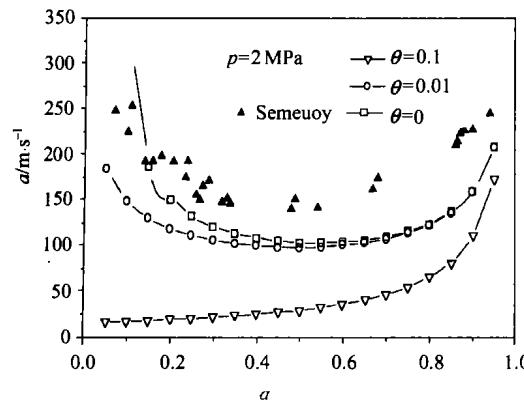


图2 与 Semeouy 实验值的比较

### 3 两相流超音速流动

两相流体的音速受其压缩性的影响, 而大大的小于任何一种单相流体, 在两相空泡率接近 50% 时。其值仅几十米每秒。低音速使两相流可在低速下达到超音速。当忽略相滑移, 不考虑壁面换热与摩擦, 考虑截面变化、相变时, 描述两相流动的基本方程如下,

$$\frac{d}{dz} [\rho_v \alpha u + \rho_l (1 - \alpha) u] = 0 \quad (2)$$

$$\frac{d}{dz} [\rho_v \alpha A u^2 + \rho_l (1 - \alpha) A u^2] = -\frac{d(pA)}{dz} \quad (3)$$

$$\begin{aligned} & \frac{d}{dz} [\rho_v \alpha u (h_v + gz + \frac{u^2}{2}) + \rho_l (1 - \alpha) u \times \\ & (h_l + gz + \frac{u^2}{2})] = 0 \end{aligned} \quad (4)$$

下标 l, v 分别代表液相、汽相参数;  $\alpha$ , 空泡率;  $u$ , 速度;  $A$ , 流道截面积。以上方程结合流道尺寸、相变换热方程, 可以求解沿流道速度、压力和马赫数分布。

作者分别对缩放流道和渐缩—等截面流道内的饱和蒸汽与过冷水的两相流动进行了计算。计算表明, 在缩放流道和渐缩—等截面流道中可能实现跨音速流动, 但是马赫数不高, 流道尺寸、流体参数和相间热交换情况对能否实现从亚音速向超音速的转变影响较大。如图3和图4所示, 两相流动由于流道截面缩小的加速作用和音速的降低, 马赫数逐渐增大, 在临界截面处, 流动达到音速, 马赫数继续增加达到超音速流动。

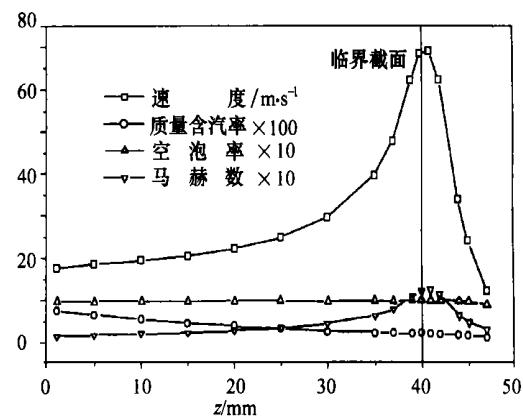


图3 缩放流道内的跨音速流动

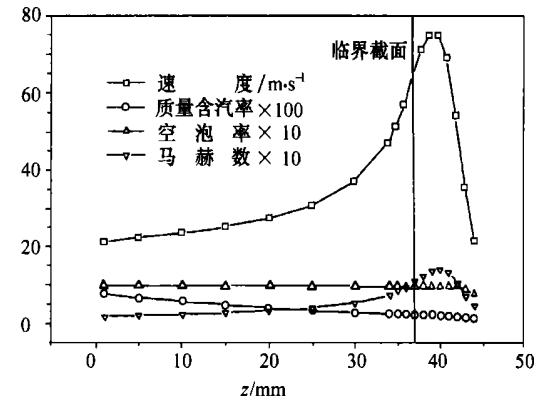


图4 渐缩—等截面流道内的跨音速流动

### 4 汽液两相流激波

对于两相流激波, 文献[2] 建立了数学模型并进行了分析, 得出了激波前后参数变化, 并对过程的熵, 可用能的变化进行了分析。在均相假定下, 忽略摩擦等的影响, 数学模型如下。

质量守恒方程:

$$[\rho_v \alpha u + \rho_l (1 - \alpha) u]_b = [\rho_v \alpha u + \rho_l (1 - \alpha) u]_a \quad (5)$$

动量方程:

$$[\rho_v \alpha u^2 + \rho_l (1 - \alpha) u^2]_a - [\rho_v \alpha u^2 + \rho_l (1 - \alpha) u^2]_b = p_b - p_a \quad (6)$$

能量守恒方程:

$$\begin{aligned} & [\rho_v \alpha u (h_v + \frac{u^2}{2}) + \rho_l (1 - \alpha) u (h_l + \frac{u^2}{2})]_b = \\ & [\rho_v \alpha u (h_v + \frac{u^2}{2}) + \rho_l (1 - \alpha) u (h_l + \frac{u^2}{2})]_a \end{aligned} \quad (7)$$

式中, 下标 b, a 分别代表激波前后的参数, v, l 分别代表蒸汽及液体的参数。基于以上模型, 以水及水蒸气为工质, 进行了数值模拟。

气混合物为例,通过计算得到两相流激波的升压特性及参数变化。

波前参数对波后参数有较大影响,当其它参数不变时,对不同波前空泡率的两相流激波的最高升压比进行了分析计算,结果如图5所示。从图中可知,当波前空泡率为50%左右时,波前马赫数较高,波后的最高升压比较大。

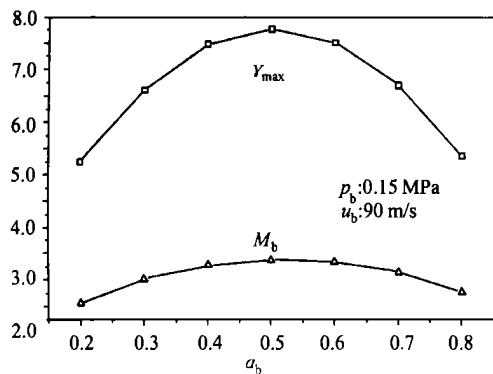


图5 不同波前空泡率下的最高升压比

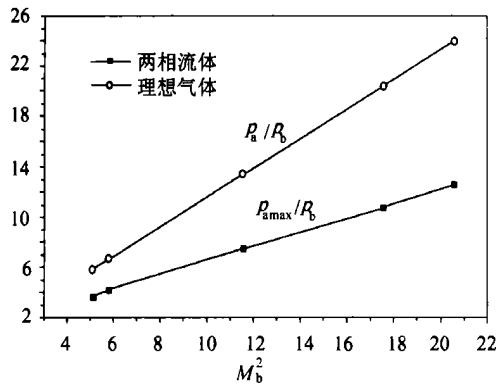


图6 最高升压比与波前马赫数的关系

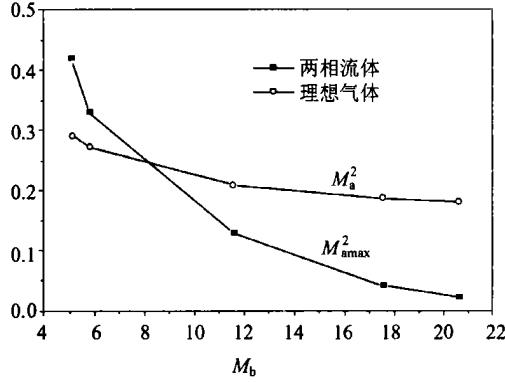


图7 波后马赫数与波前马赫数的关系

图6分别给出了理想气体和两相流体激波的升压比与波前马赫数平方  $M_b^2$  的关系,对两相流体升

压比采用了最高升压比。两相流体最高升压比与  $M_b^2$  经拟合呈近似线性变化关系,用  $\gamma_{\max}$  代表最高升压比,其关系为,

$$\gamma_{\max} = p_{\max}/p_b = 0.57M_b^2 + 0.786 \quad (8)$$

图7分别给出了两相流体和理想气体的波后马赫数与波前马赫数之间的关系。经拟合,可得如下关系式,

$$M_a^2 = (2.0068 - 0.0488M_b^2)/(1.1217M_b^2 - 0.0510) \quad (9)$$

$M_{\max}$  为最高升压比对应波后马赫数。

对激波前后熵和可用能的进一步分析发现,激波后的熵增加,可用能减少。

## 5 两相流激波的应用

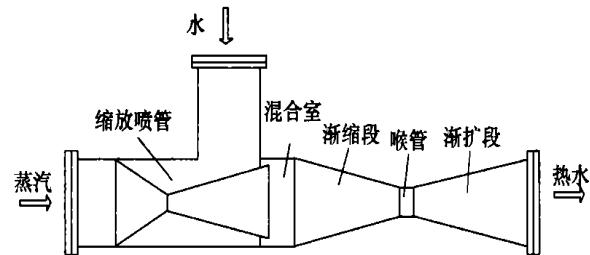


图8 增压换热器结构简图

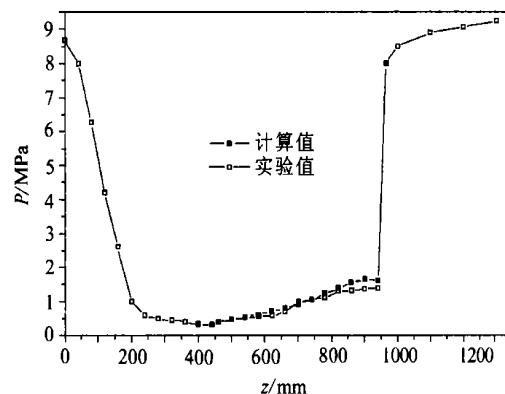


图9 压力分布与实验值的比较

利用两相流的音速特点,并结合激波使汽相具有凝结、压力升高的特点,借此设计一种汽水直接接触式增压换热器(图8)。该装置为汽水引射混合式换热器,以蒸汽为引射流体,水为被引射流体,也可以水为引射流体,蒸汽为被引射流体,两种流体

混合后, 蒸汽与水充分接触并进行换热, 汽相凝结, 水温升高, 出口时蒸汽完全凝结为热水。同时, 由于流体在流道内处于超音速流动状态, 受背压等的影响, 在流道中产生激波, 激波同时使汽相凝结加快, 也使流体的压力升高, 从而达到高效换热和增压的目的。

作者利用所建数学模型对两相流动和激波进行了计算<sup>[3]</sup>, 并与 Cattadori<sup>[4]</sup> 的实验结果进行了比较, 如图 9 和图 10 所示。从图 9 可知, 计算值与实验值吻合较好。图 10 为相应的速度  $u$  和马赫数  $M$  分布计算结果。

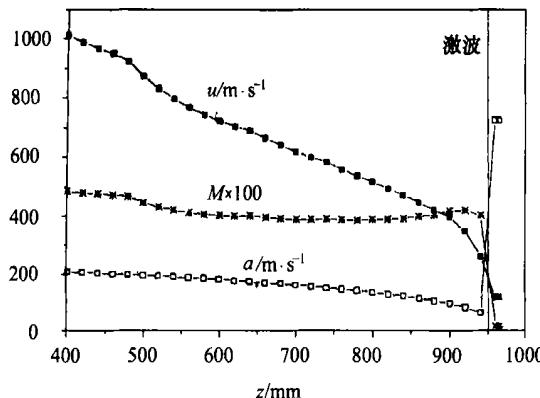


图 10 混合段的速度和马赫数分布

## 6 结论

(1) 两相流体的音速受可压缩性影响而呈现出与单相流不同的特点, 其值大大低于单相流体音速值。同时不可逆因素对音速的影响随频率的增加而增加, 在高频时需考虑导热、粘性和相变对音速的影响, 在低频时应主要考虑相变对音速的影响;

(2) 两相流在缩放流道和渐缩—等截面流道中可能实现跨音速流动;

(3) 对汽液两相流激波, 其波后的参数与相变的强弱密切相关, 相变越强、激波后的压力越高, 在汽相完全凝结时激波最强, 达到最大的压力升高比, 波后最高升压比与波前马赫数平方呈近似线性关系;

(4) 两相流音速和激波特点, 可设计增压高效换热器, 同时实现高效换热和增压。

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**狭缝通道两相流强化换热研究综述=A Overview of the Intensified Heat Exchange Research of Two-phase Flows in a Narrow-gap Channel** [刊, 汉] / WANG Zeng-hui, JIA Dou-nan, LIU Rui-lan (Nuclear & Thermal Energy Engineering Department, Xi'an Jiaotong University, Xi'an, China, Post Code: 710049) // Journal of Engineering for Thermal Energy & Power. —2002, 17(4): 329 ~ 331, 335

Under the sweep action of a high-speed fluid in a narrow gap channel the narrow gap is immune from foreign matter sedimentation which may pollute heat transfer surfaces, resulting in a deterioration of the heat transfer conditions. Narrow-gap two-phase heat transfer technology features a compact structure and, endowed with remarkable intensification effectiveness, represents a kind of both economical and effective intensified heat transfer method. Hence, the narrow gap heat transfer has been widely utilized in various engineering sectors, such as aerospace and aeronautics, microelectronics and nuclear reactors. The main heat transfer mechanism of the above-cited heat transfer is based on the micro-liquid film evaporation at the bottom of pressured and deformed gas bubbles. The authors have given a brief account of the research progress made in the area of two-phase flow intensified heat transfer in a narrow-gap channel with an overview of the present status of the on-going study. **Key words:** narrow-gap channel, micro-film evaporation, intensified heat transfer

**两相流超音速流动、激波及其应用研究=A Study of Two-phase Flow Supersonic Flows Shock Waves and Their Applications** [刊, 汉] / ZHAO Liang-ju, ZENG Dan-ling (College of Power Engineering, Chongqing University, Chongqing, China, Post Code: 400044) // Journal of Engineering for Thermal Energy & Power. —2002, 17(4): 332 ~ 335

On the basis of the specific features of two-phase fluid sonic speed a study was conducted of two-phase supersonic flows followed by an analysis of the shock waves triggered by the supersonic flows. Moreover, by the use of the features of two-phase shock-wave accelerating condensation and pressure rise designed is a supercharged heat exchanger. The sonic speed of two-phase flows under the influence of its compressibility presents some features different from those of single-phase flows. Their relatively low sonic speed makes it easier to realize two-phase supersonic flows. The two-phase flow shock waves are closely related to wave-front Mach number. Wave-rear vapor condensation results in a pressure rise. A steam-water direct-contact heat exchangers designed by exploiting the above-mentioned feature is characterized by a high-efficiency heat exchange and pressure charging. **Key words:** vapor-liquid two-phase flow, supersonic flow, shock wave, supercharged heat exchanger

**利用 T 型三通测量气液两相流体的流量和干度=Measurement of Flow Rate and Dryness of a Vapor-liquid Two-phase Fluid by Using a T-junction** [刊, 汉] / WANG Dong, LIN Yi, LIN Zong-hu (Energy and Power Engineering Department, Xi'an Jiaotong University, Xi'an, China, Post Code: 710049) // Journal of Engineering for Thermal Energy & Power. —2002, 17(4): 336 ~ 338, 348

Through the use of the phase separation features of a T-junction a portion of single-phase gas stream is extracted and separated from a measured gas-liquid two-phase fluid. By the measurement of this portion of the single-phase gas flow rate determined is the flow rate or dryness of the measured gas-liquid two-phase fluid. The specific feature of this method lies in the conversion of flow rate measurement of a two-phase fluid into the measurement of a single-phase fluid, resulting in a significant improvement of instrumentation stability and reliability and a remarkable enhancement of measurement precision. Test results indicate that the flow extraction ratio is directly proportional to the dryness of the measured two-phase flow. Within the test range adopted by the authors the average measurement error of flow rate and dryness is less than  $\pm 5\%$ . **Key words:** flow meter, two-phase flow, T-junction, flow extraction and separation

**分层协同进化模型在热力系统在线优化中的应用研究=Applied Research of a Multi-tier Synergetic Evolution Model in the On-line Operation Optimization of a Thermodynamic System** [刊, 汉] / WANG Xin-xin, XU Xiang-dong (Department of Thermal Energy Engineering, Tsinghua University, Beijing, China, Post Code: 100084) // Journal of Engineering for Thermal Energy & Power. —2002, 17(4): 339 ~ 341