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# HS-A 柴油机燃料油技术研究

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摘 要: 在柴油机燃料油各种节油和替代技术中, HS—A柴油机燃料油可以替代0号柴油应用在高、中、低速柴油机和各种柴油燃烧器上。 文中介绍了该油的研制过程, 如残炭值的变化, 以及试验情况。该油料合成工艺简单, 投资及合成成本低

关键词: 柴油机燃料油;替代技术;化学添加剂;试验研究

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# 1 引言

随着柴油用量的增加,人们越来越重视柴油的节油替代技术研究。节油技术有在柴油中加 10%左右水和乳化剂的乳化柴油技术,但是由于乳化油存在不稳定因素,经常有破乳现象发生,使水与油分离,无法正常燃烧。替代技术中有重质燃料替代柴油,在低速发动机上应用。主要有日本 Nikko 公司采用生物催化剂达到重油轻质化目的的专利技术及美国重油中加萜烯化合物通过超声波反应器达到轻质化的专利技术等。这些技术的生产工艺复杂,投资巨大,生产成本高,推广起来比较困难。

1999年笔者开始研制 HS-A 柴油机燃料油替代柴油技术。

## 2 HS-A 柴油机燃料油理论研究

结合我国实际情况对技术资料进行分析,并考虑了理论上的可行性和经济上的适用性,设想以重油为基础,加入少量的柴油和化学添加剂合成一种新型柴油机燃料油。重油是原油提炼出汽油、柴油等油品后的渣油。它具有粘度高、流动性差、闪点高、可燃烧性差、密度高、杂质多、含硫量高和沥青含量高等特点。我们分析了重油的化学成分,重油中主要元素是: C 为 85%~88%, H 为 12%~13.6%,

其它元素为  $0.5\% \sim 1.0\%$ 。 C 和 H 都是可燃元素,其反应式为  $C+O_2=CO_2+408$  kJ,  $H_2+0.5O_2=H_2O_2+206$  kJ。氢碳原子数比  $(H/C)_a$  和氢碳质量比  $(C/H)_m$  是评价油品的重要指标, $(H/C)_a$  值愈高, $(C/H)_m$  值愈低,则油品愈好。这样我们大胆设想,在重油中加入一定比例的化学添加剂,使  $(H/C)_a$  值增加, $(C/H)_m$  值下降,达到降低闪点、增加热值、降低密度和粘度、提高油品的流动性能的目的。为使180号重油转变为替代 0 号柴油的 HS-A 柴油机燃料油,我们研制了化学添加剂,把它加入 180 号重油和柴油中,合成的 HS-A 柴油机燃料油完全能够替代 0 号柴油使用。

# 3 HS-A 柴油机燃料油化学添加剂的研究

# 3.1 氢碳比的研究

在化学添加剂中,以加氢剂为主,同时加入少量的防腐剂和脱硫剂,如:铝、钡、镁、锰等盐类和氧化物。

加氢剂主要是金属元素,有周期表 VII族的全部金属和 Ib 组的铜, VIII 族铼的等,也可以是 VIIa 族的钼、钨和氟化碱金属的镍或碱土金属的硅铝酸盐等进行反复试验,寻找适合重油的加氢剂,做为化学添加剂的主要元素。在试验中对几十种化学元素及化合物进行分析、比较,又对近百个化学方程式分析、计算,最后优选了主要化学成分有: A、B、C、D 作为加氢剂的主要成分。通过正交设计法试验分析,得出对增加(H/C)a 值的结果。

选定主要元素: A、B、C、D。

确定(H/C)a 值变化的值为:

- (1)(H/C)。值在 1.6~1.64 范围;
- (2) (H/C)a 值在 1.64~1.67 范围;
- (3)(H/C)。值在 1.67 以上。

这样对 4 个元素、3 个范围的问题, 选用正交表

### L9(3)来安排试验,试验结果见表 1。

表1 正交表 19(3)

	1(A)	2(B)	3(C)	4(D)	(H/C)a	减去1.6
	I(A)	2(B)	3(4)	4(D)	(II/ C/a	乘 100
1	1	1	1	1	1.6	0
2	1	2	2	3	1.62	2
3	1	3	3	2	1.67	7
4	2	1	2	3	1.65	5
5	2	2	3	1	1.66	6
6	2	3	1	2	1.63	3
7	3	1	1	2	1.61	1
8	3	2	3	3	1.69	9
9	3	3	2	1	1.68	8
K1	9	6	4	14		
K2	14	17	15	11		
K3	18	18	22	16		
K1/3	3	2	1. 33	4. 67		
K2/3	4.67	5.67	5	1.67		
K3/3	6	6	7. 33	5. 33		
极差	3	4	6	3.66		
优选方案	A 3	B2	C3	D4		

四个级差 3、4、6、3.66 中最大的是 6, 说明 C 对试验指标影响最大。第 8 号试验中(H/C)a 值为1.69, 接近柴油(H/C)a 值1.72, 元素 1(A)、3(C)、4(D)都是最佳水平, 元素 2(B)也在比较好的水平上。由此第 8 号试验元素为最佳方案。接着又测试了 C成分在重油中的作用,即对(H/C)a 值和(C/H)m 值的影响, 见表 2 和图 1。

### 3.2 降低残炭的研究

在化学添加剂中加入除炭剂 E, 以解决重油残炭高的问题, 现就除炭剂 E 对残炭的影响进行测试分析。设x 为除炭剂 E 的百分比含量, y 为残炭值。测得数据列于表 3, 根据测试数据绘出坐标图, 见图 2。

表 2 重油加 C 成分后对氢碳比的影响

C 成分/ %	含C/ %	含 H/%	(H/C)a	(C/H)m
1. 0	84. 1	11.3	1.61	7.44
1. 2	84. 1	11.6	1.65	7.25
1. 4	84. 1	11.8	1.68	7.13
1. 6	84. 1	12.3	1. 73	6.95
1. 8	84. 1	12.3	1. 76	6.83

表3 E与残炭关系

序号	х	у
1	0.4	6.52
2	0.6	5.36
3	0.8	4.33
4	1.0	3.58
5	1.2	2.96
6	1.4	2.38
7	1.6	2.05
8	1.8	1.68
9	2.0	1.42
10	2. 2	1.31

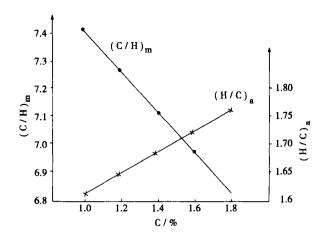


图1 重油加C成分后(H/C)a和(C/H)m的变化

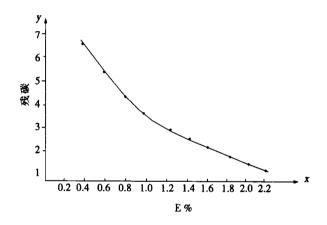


图 2 E 与残炭关系 曲线

从坐标图可以看出,随着 E 比例的增加,残炭值随着下降,则y与x为反比例函数关系,设表达式为:y=a+b/x,求出回归曲线方程,计算结果见表4。

表 4 回归曲线计算表

	$\chi_i$	$M_i = 1/x$	$y_i$	$M_i y_i$	$M_i^2$	$y_i^2$
1	0.4	2.5	6.25	16. 3	6. 25	42. 51
2	0.6	1.67	5.36	8.95	2. 79	28.73
3	0.8	1. 25	4.33	5. 41	1.56	18.75
4	1.0	1.0	3.58	3.58	1	12.82
5	1.2	0.83	2.96	2.46	0.69	8.76
6	1.4	0. 71	2.38	1. 69	0.5	5.66
7	1.6	0.63	2.05	1. 29	0.4	4. 20
8	1.8	0.56	1.68	0.94	0.31	2.82
9	2.0	0.5	1.42	0.71	0.25	2.02
10	2. 2	0.45	1.31	0.59	0.2	1.72
Σ	13	10.10	31. 59	41.92	13. 95	127.99

将 y = a + b(1/x), 变为直线回归方程, 取 n = 10.

$$\overline{M} = \sum_{i=1}^{n} M_{i}/n = 10.1/10 = 1.01$$

$$\overline{y} = \sum_{i=1}^{n} y_{i}/n = 31.59/10 = 3.159$$
再代入:
$$b = (\sum_{i=1}^{n} M_{i}y_{i} - \overline{M} \circ \sum_{i=1}^{n} y_{i})/(\sum_{i=1}^{n} M_{i}^{2} - \overline{M} \circ \sum_{i=1}^{n} M_{i}) = (41.92 - 1.01 \times 31.59)/(13.95 - 1.01 \times 10.1) = (41.92 - 31.91)/(13.95 - 10.2) = 2.66$$

$$a = \overline{y} - b\overline{M} = 3.159 - 2.67 \times 1.01 = 0.462$$
得直线回归方程为:  $y = 0.462 + 2.67M$ 

$$M = \frac{1}{r}$$
代入上式得:  $y = 0.462 + 2.67\frac{1}{r}$ 

#### 降低闪点的研究 3.3

为除炭剂 E 与残炭值的回归曲线方程。

应用正交设计法,对降低闪点进行反复试验,在 添加剂中加入降低闪点的成分F。设X为降低闪点 成分F 的百分比,Y 为闭口闪点。通过降低闪点试验 得到的回归曲线方程数据(见表5)。

表 5 测试 F 对闭口闪点的回归方程

	$X_i$	$Y_{i}$	$X_i^2$	$Y_i^2$	$X_iY_i$
1	0. 5	109	0. 25	11 881	54. 5
2	0.8	101	0.64	10 201	80.8
3	1.1	91	1. 21	8 281	100.1
4	1.4	83	1.96	6 889	116.2
5	1.7	74	2. 89	54 765	125.8
6	2.0	65	4	4 225	130
$\sum$	7.5	523	10. 95	46 953	607.4

根据测试数据得出坐标图(见图3)。

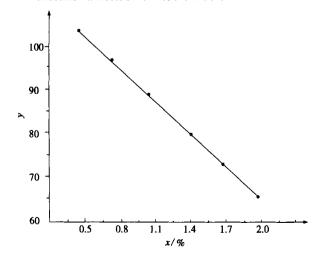


图 3 加剂量与闭口闪点坐标图

回归系数计算如下:

$$\sum_{i=1}^{N} X_i = 7.5, \quad \sum_{i=1}^{N} Y_i = 523, \quad N = 6$$

$$\overline{X} = 1.25, \overline{Y} = 87.17,$$

$$\sum_{i=1}^{N} X_i^2 = 10.95, \quad \sum_{i=1}^{N} Y_i^2 = 46.953, \quad \sum_{i=1}^{N} X_i Y_i = 607.4$$

$$\frac{\frac{1}{N} (\sum_{i=1}^{N} X_i)^2}{L_{XX}} = \frac{9.38}{1.57}, \quad \frac{\frac{1}{N} (\sum_{i=1}^{N} Y_i)^2}{L_{YY}} = \frac{45.588.17}{1.364.83},$$

$$\frac{\frac{1}{N} (\sum_{i=1}^{N} X_i) (\sum_{i=1}^{N} Y_i)}{L_{XY}} = \frac{653.75}{-46.35}$$

$$b = \frac{L_{XY}}{L_{XX}} = \frac{-46.35}{1.57} = -29.52$$

$$a = \overline{Y} - b\overline{X} = 87.17 - (-29.52) \times 1.25$$

$$= 124.07$$

则回归直线方程为: Y = 124.07 - 29.52X判断X,Y之间的明显性.

拟定检验水平 a=0.01, 变量的个数等于 2, 误 差自由度为 7, 则  $\lambda = 0.798$ 。

$$U = bL_{XY} = (-29.52) \times (-46.35) = 1368.25$$
 
$$| \gamma_{ii} | = \sqrt{\frac{U}{L_{YY}}} = \sqrt{\frac{1368.25}{1364.83}} = 1.001$$
 因为  $| \gamma_{ii} | = 1.001 > 0.798 = \lambda$  所以  $X = Y$  之间的线性相关关系是明显的。

通过试验研究,得出化学添加剂最佳组份为.加 氢剂 42%、除炭剂 E 为 26.5%、降闪点剂 F 为 24%、 降硫降沥青质等成分为 7.5%。

# 4 HS-A 柴油机燃料油研究

经过实验室大量试验,数据整理与分析后,确定 了HS-A 柴油机燃料油的配方: 180 号重油为 63 %, 化学添加剂为5%,柴油为32%。通过试验测得HS ─A 柴油机燃料油与柴油中的氢碳原子数比(H/ C)a, 碳氢质量比(C/H)m 随密度 ₽的变化关系(见图 4), 进一步证实了通过加氢剂的有效作用, 使 HS-A 柴油机燃料油的(H/C)a 和(C/H)m 接近柴油。

表 6 HS-A 柴油机燃料油、0 号柴油、重柴油技术指标

	0号柴油	重柴油	HS-A 柴油机燃料油
			木川川州
运动粘度/mm <sup>2</sup> °s <sup>-1</sup>	3 ~ 8(20 ℃)	36. 2(50 °C)	13. 8(50 ℃)
密度/g°cm <sup>-3</sup> (20℃)	0.84	0.91	0. 90
闪点(闭口)/ ℃	65	65	65
残炭/ %	0.4	1.5	1.32
灰分/ %	0.02	0.04	0.026
凝点/ ℃	0	13	0

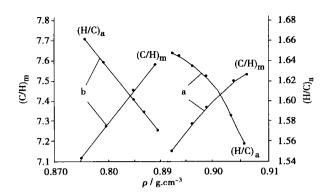


图 4 HS-A 柴油机燃料油(a)与柴油(b)中 (H/C)a、(C/H)m 随密度 θ 的变 化

检测 HS-A 柴油机燃料油、0 号柴油、重柴油的技术指标,数据见表 6。

从表中可以清楚的看到 HS-A 柴油机燃料油技术指标在 0 号柴油和重柴油之间,是可替代柴油的新型燃料油。

# 5 应用试验及长期可靠性测试

HS-A 柴油机燃料油在松花江中的小型轮船上进行试验,其发动机为 S2100 型。试验过程中发动机运行良好,测试数据与柴油接近。又在香港"伟高"轮捷克产 700 kW 发动机和江苏苏泰兴渔 2105号等多条轮船上试用 HS-A 柴油机燃料油,都取得了很好的效果。

为检验 HS-A 柴油机燃料油运行的长期可靠性和在远洋船舶应用的可能性,交通部船舶运输节能技术服务中心和交通部上海船舶运输科学研究所在 6 135 Ca 柴油机上进行了 360 h 连续可靠性试验。试验着重对以下方面进行测试:

- (a) 6 135 Ca 柴油机性能测试。试验表明: 6 135 Ca 柴油机使用 HS—A 柴油机燃料油时,对柴油机转速和功率没有影响。柴油机的稳定性与使用柴油基本相同。
- (b) 6135Ca 柴油机启动试验。在常温下,柴油机能够依次顺利启动。
- (c) 运行可靠性试验。柴油机连续运行 360 h 没有更换喷油嘴,喷油压力没有降低,燃油过滤器滤芯未见破损,润滑油使用寿命可以保持在推荐时间内(300~500 h),柴油机运行中未发生异常情况。
- (d) 柴油机燃烧室积炭检查。柴油机连续运行360 h 后, 观察燃烧室喷油嘴、活塞顶、排气阀等积炭情况。气缸盖燃烧室内有少许正常积炭, 喷油嘴和活塞顶部的积炭与柴油机使用柴油的情况没有明显差别。

试验结果表明:高、中、低速柴油机可以使用 HS — A 柴油机燃料油,高压油泵柱塞不会出现咬死,喷油嘴不会堵塞,推进特性平均增加 1.89%,负荷特性平均增加 4.85%,运行安全可靠。

HS-A 柴油机燃料油技术合成工艺简单,采用 先进、全封闭的静态混合装置,保证各组分均匀混合,该燃料完全可以替代0号柴油在各种高、中、低速柴油机上应用,也可在各种柴油燃烧器上使用。

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## (上接第416页)

针对原有烧劣质油的机组,可以在原来的点火器位置用该系统替代。由于系统结构简单而紧凑,改装工作量小,适合于在国内燃机应用领域推广。使用时应注意:检查高压电缆的完好性,电源接地情况,系统绝缘性能以及电极间的间隙;检查系统工作能力。通电后,电极间应产生脉冲放电电弧,频率符合要求且稳定;严禁操作人员在系统处于工作状态下,打开电源箱箱盖或接触高压屏蔽电缆;禁止该系统

与腐蚀性物质(化学药品,酸和碱等)一起保管;禁止引起锈蚀的气体及水等其它液体进入电源箱。

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process a local thermodynamic-balance fluid model was employed with SIMPLEC algorithm being used for a numerical scheme. A curvilinear coordinate system was put into use for a mesh model. A distribution diagram showing the variation of temperature and speed field and constituent elements was provided by the calculation results. **Key words:** plasmanumerical simulation, chemical reaction, local thermodynamics equilibrium

用资源的观点评价能源利用项目— Evaluation of Energy Resource Utilization Projects from the Viewpoint of Resources [刊,汉]/YE Han-dong, LI Yu-hong, YE Da-jun (Tsinghua University, Beijing, China, Post Code: 100084)//Journal of Engineering for Thermal Energy & Power.— 2003, 18(4).—407~410

During the evaluation of energy resource utilization projects a comprehensive evaluation method should be used with technical, economic, environmental and other related factors being taken into account. The authors have described a comprehensive evaluation method based on a total resource system. Under this method air, water and fuel, etc consumed (including those expended by pollution) in production are converted into material resources. Moreover, from the viewpoint of social-average marginal cost-cut calculated is the external cost to the society due to the utilization of resources. It is noted that during the calculation of resource values the external cost must be included and be listed into the final total cost. Furthermore, the principles of this comprehensive evaluation method are also expounded. A combined cycle cogeneration power plant involving a natural gas-fired gas turbine is compared with a coal-fired cogeneration power plant system. The results of this comparison demonstrate that the evaluation of power projects from the viewpoint of resource utilization is fully justified. **Key words**; total resources, comprehensive evaluation, energy-based power project, environment

火炬气在燃煤锅炉上的回收利用研究—An Investigation on the Recycling of Flare Gas for Use in a Coal-fired Boiler [刊,汉] / CHAI Qin-hu, DING Yan-jun (Tsinghua University, Beijing, China, Post Code: 100084), ZHANG De-hua, ZHANG Wen-wu (Thermal Power Plant of Yangtze Petrochemical Co. Ltd., Nanjing, China, Post Code: 210048) //Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —411~414

Through a specific retrofit example the problem of flare gas recycling for use in a coal-fired boiler is analyzed with the impact of mixed burning of coal and flare gas on the boiler operating characteristics being tested and probed. It is noted that, depending on the volume flow of flare gas and its specific properties, one must adjust accordingly the air distribution mode and optimum excess air factor, etc with a view to achieving satisfactory results in this recycling effort. **Key words:** coal-fired boiler, flare gas, recycling unit

等离子点火系统在燃气轮机上的应用= The Use of Plasma Ignition Systems in Gas Turbines [刊,汉] / HAN Li-zhong, CHEN Hong-fa, CHEN Yan-fen (Harbin No. 703 Research Institute, Harbin, China, Post Code: 150036), ZENG Xi (Chinese Navy Military Representative Office at No. 436 Factory) //Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —415~416

The composition, working principles and usage effectiveness of a plasma ignition system are described. As compared with other electric-spark ignition units, the plasma ignition system features high electric-discharge energy, dirt resistance, and particularly a combustion intensification function during ignition. Some requirements regarding the system configuration for different engine units are analyzed, and several issues meriting close attention during operation also presented. **Key words:** gas turbine, combustor, plasma

HS—A 柴油机燃料油技术研究—Technical Study of HS-A Diesel Engine Fuel Oil [刊,汉] / WANG Zhi-cherg, CAO Zhi-de, ZHANG Hong-qi (Heilongjiang Provincial Energy Source Environment Research Academy, Harbin, China, Post Code; 150090) //Journal of Engineering for Thermal Energy & Power, 1—2003, 18(4). —417~420 only not

Concerning various oil-saving and alternative technologies for diesel engine fuel oil it is noted that HS-A diesel oil can replace No. 0 diesel oil for use in high, medium and low-speed diesels and various diesel oil burners. The combustion mechanism and the variation of residual carbon value of the HS-A diesel oil are analyzed and some test conditions given. The synthesis technology of the above-mentioned oil features a simplified process, low investment and production cost. **Key words:** diesel engine fuel oil, alternative technology, chemical additive, experimental research

125 MW 机组锅炉给水泵液力偶合器损坏原因分析—An Analysis of the Causes Leading to the Damage of the Fluid Couplings of Boiler Feedwater Pumps for a 125MW Power plant [刊,汉]/ LIU Gui-ping, LI Xian-bao (Jiaozuo AES Wanfang Power Plant, Zuozu, China, Post Code: 454172), JI Li-gang (Jiaozuo Brake Co. Ltd., Jiaozuo, China, Post Code: 454000) // Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —421 ~ 422

In a period of less than three months the fluid couplings of two boiler feedwater pumps for a 125MW unit had all broken down due to a furnace flame-out caused by boiler slag drop-thumping. A detailed analysis has shown that the failure condition and component damage are identical for each of the two cases of the coupling failure. The main cause can be attributed to an excessively high operating oil temperature of the couplings, which has exceeded the fusion temperature (130 °C) of the tungalloy of the coupling component. In view of the above, several measures were proposed to deal with the situation, such as a reduction of the coupling operating oil temperature, a lower speed adopted for conducting boiler load increase and decrease, a moderate range of adjustment for the coupling flow-guide tube, etc. The introduction of the above measures has resulted in an enhancement of the feedwater pump unit service life as well as the safety and economic operation of the boiler units. **Key words**: 125MW power plant, fluid coupling, flow-guide tube of a coupling

T91/P91 钢管在电站锅炉应用中的质量控制=Quality Control of T91/P91 Steel Tubes Used in Utility Boilers [刊,汉] / YU Xiu-qing, CHEN Li-peng, CHEN Jia-lun (Harbin Boiler Co. Ltd., Harbin, China, Post Code; 150046) // Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —423~425

In conjunction with specific conditions of boiler fabrication T91/P91 steel tubes have been widely used for manufacturing utility boilers. The requirements of quality index control during the production process are discussed, which cover such a variety of aspects as raw materials, welding, heat treatment, cold and hot working, etc. **Key words:** raw materials, welding, heat treatment

VN 技术在容克式空气预热器密封改造中的应用— The Use of VN (Vertical Layout of Air Heater and Nonadjustable Seal Partition Plate) Technology in the Technical Modification of Seals for Ljungstrom Regenerative Air Heaters [刊,汉] / GONG Han—qiang (Shengli Power Plant, Jinan, China, Post Code: 257087) //Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —426~427

**Key words:** air heater, VN (vertical layout of air heater and nonadjustable seal partition plate) technology, Ljungstrom air heater, seal modification

"曙光—机器设计"燃气轮机制造科研生产联合体="Machine Design - Aurora" - A Ukraine-based Gas Turbine Manufacturing Enterprise Known for its Integration of Scientific Research with Production [刊, 汉] / TIAN Guang, KOU Dan, JI Gui-ming (Harbin No. 703 Research Institute, Harbin, China, Post Code; 150036) // Journal of Engineering for Thermal Energy & Power. — 2003, 18(4). —428~429